

Mapping surface displacement using a pair of interferograms: a comparative study

S. Dumont^{1,2}, F. Sigmundsson¹, F. Lopes³

1 Institute of Earth Sciences, University of Iceland, Reykjavík, Iceland

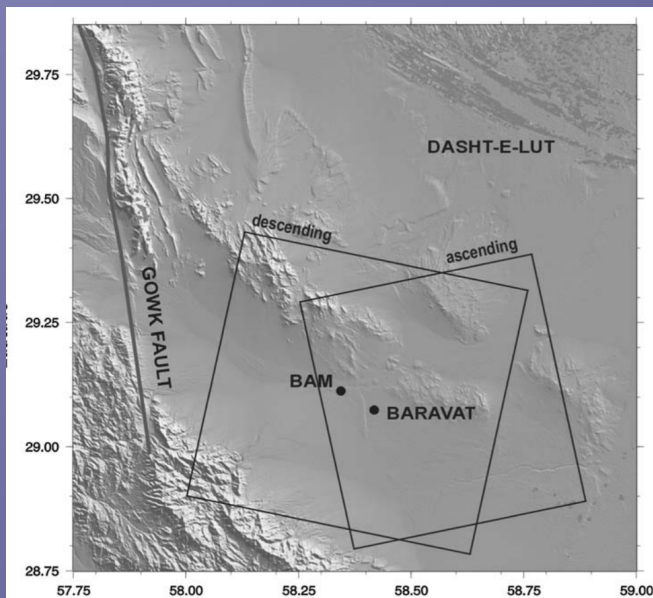
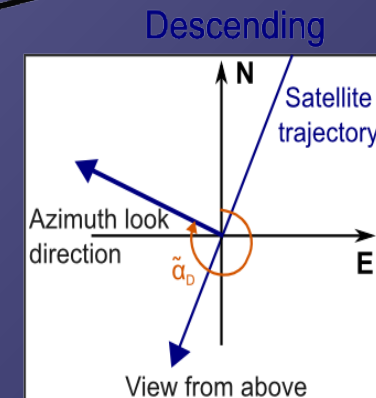
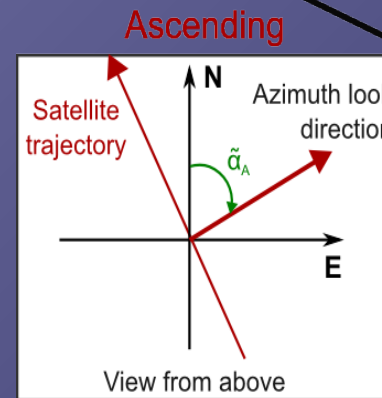
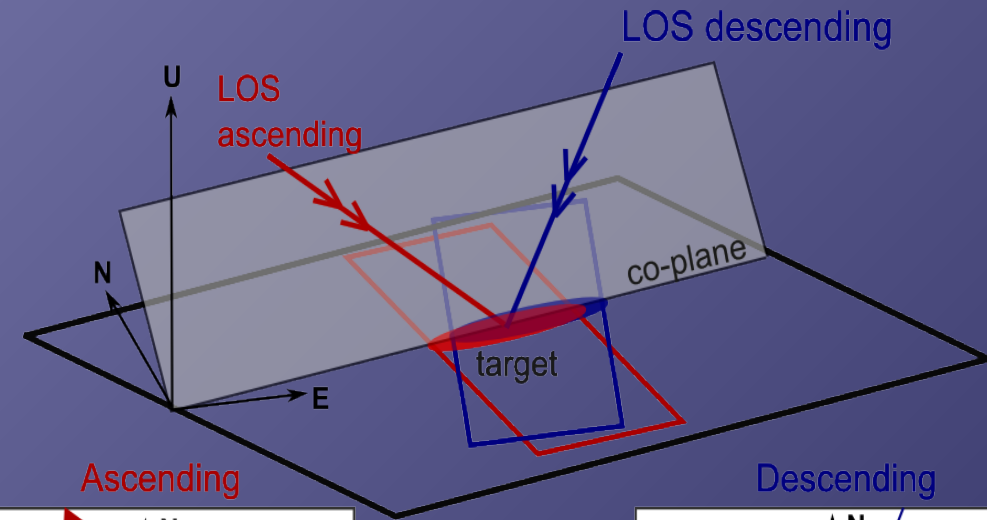
2 IDL, University of Beira Interior, Covilhã, Portugal

3 Institut de Physique du Globe, Paris, France



Introduction

- InSAR analysis → 1D measurement: projection of the surface deformation field into the Line-of-sight (LOS)
- To resolve the 3D deformation field with standard InSAR techniques, a combination of at least 3 interferograms acquired with different imaging geometries is required
- However, most areas are regularly imaged by two configurations: one ascending, one descending



Introduction

Equation system defined for a pair of interferograms

$$\begin{pmatrix} d_{ASC} \\ d_{DESC} \end{pmatrix} = \begin{pmatrix} -\sin(\theta_A) \sin(\tilde{\alpha}_A) & -\sin(\theta_A) \cos(\tilde{\alpha}_A) & \cos(\theta_A) \\ -\sin(\theta_D) \sin(\tilde{\alpha}_D) & -\sin(\theta_D) \cos(\tilde{\alpha}_D) & \cos(\theta_D) \end{pmatrix} \begin{pmatrix} U_e \\ U_n \\ U_{up} \end{pmatrix}$$

θ is the incidence angle, $\tilde{\alpha}_A$ and $\tilde{\alpha}_D$ are the azimuth look directions

A linear system of equations

$$\mathbf{d} = \mathbf{G}\mathbf{m}$$

Observations

Model

Decomposition approaches

- 2 component linear inversion:

Hypothesis on the nature of the deformation field: Elimination of 1 or 2 horizontal components

$$\begin{pmatrix} d_{ASC} \\ d_{DESC} \end{pmatrix} = \begin{pmatrix} -\sin(\theta_A) \sin(\tilde{\alpha}_A) & -\sin(\theta_A) \cos(\tilde{\alpha}_A) & \cos(\theta_A) \\ -\sin(\theta_D) \sin(\tilde{\alpha}_D) & -\sin(\theta_D) \cos(\tilde{\alpha}_D) & \cos(\theta_D) \end{pmatrix} \begin{pmatrix} U_e \\ U_n \\ U_{up} \end{pmatrix} \longrightarrow \begin{cases} \begin{pmatrix} d_{ASC} \\ d_{DESC} \end{pmatrix} = \begin{pmatrix} -\sin(\theta_A) \sin(\tilde{\alpha}_A) & \cos(\theta_A) \\ -\sin(\theta_D) \sin(\tilde{\alpha}_D) & \cos(\theta_D) \end{pmatrix} \begin{pmatrix} U_e \\ U_{up} \end{pmatrix} \\ U_{up} = d_{LOS} / \cos\theta \end{cases}$$

- Linear combination (LC method):

Linear combination applied on the LOS unit vectors → sensitivity to near-vertical and near-east components

$$\text{Near-Up: } \mathbf{NU} = \mathbf{d}_{DESC} + \mathbf{d}_{ASC}$$

$$\text{Near-East: } \mathbf{NE} = \mathbf{d}_{DESC} - \mathbf{d}_{ASC}$$

Objectives

- 1- Quantify the **ability to reconstruct the components of the true deformation field** using a pair of interferograms and the **model resolution matrix**
- 2- **Propose a robust method** that takes into account uncertainties of the true deformation field measurement to reconstruct the vertical and east-components using a pair of interferograms
- 3- **Compare** our approach with the classical decomposition methods

Model Resolution Matrix (MRM)

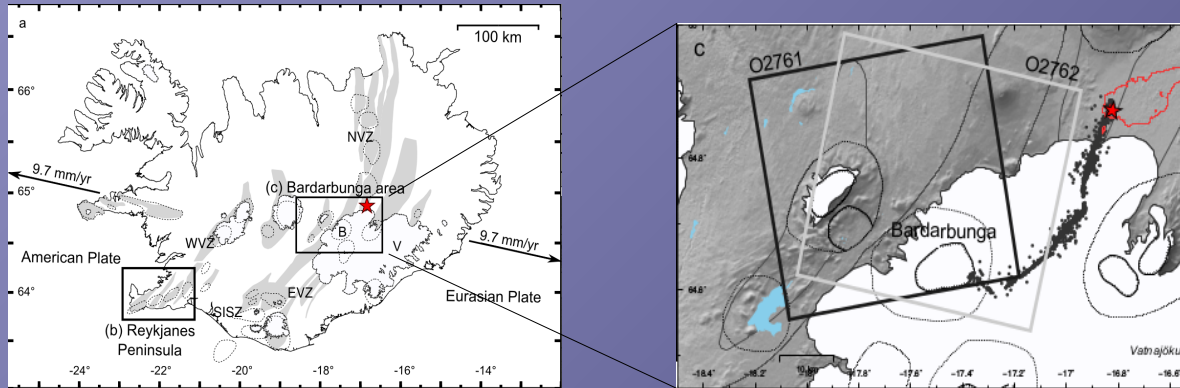
- System of acquisition (side-looking geometry) does not measure the true deformation field → it acts as a spatial filter
- Is it possible to estimate the true deformation field using the information on acquisition system (G matrix) Or is it possible to estimate an error on the component retrieval ?

$$\begin{pmatrix} d_{ASC} \\ d_{DESC} \end{pmatrix} = \underbrace{\begin{pmatrix} -\sin(\theta_A) \sin(\tilde{\alpha}_A) & -\sin(\theta_A) \cos(\tilde{\alpha}_A) & \cos(\theta_A) \\ -\sin(\theta_D) \sin(\tilde{\alpha}_D) & -\sin(\theta_D) \cos(\tilde{\alpha}_D) & \cos(\theta_D) \end{pmatrix}}_{\mathbf{G}} \begin{pmatrix} U_e \\ U_n \\ U_{up} \end{pmatrix} \Bigg\} \mathbf{m}^{est}$$

$$\mathbf{m}^{est} = [\mathbf{G}^{-g} \mathbf{G}] \mathbf{m}^{true} = \mathbf{R} \mathbf{m}^{true}$$

↑
Inverse general matrix

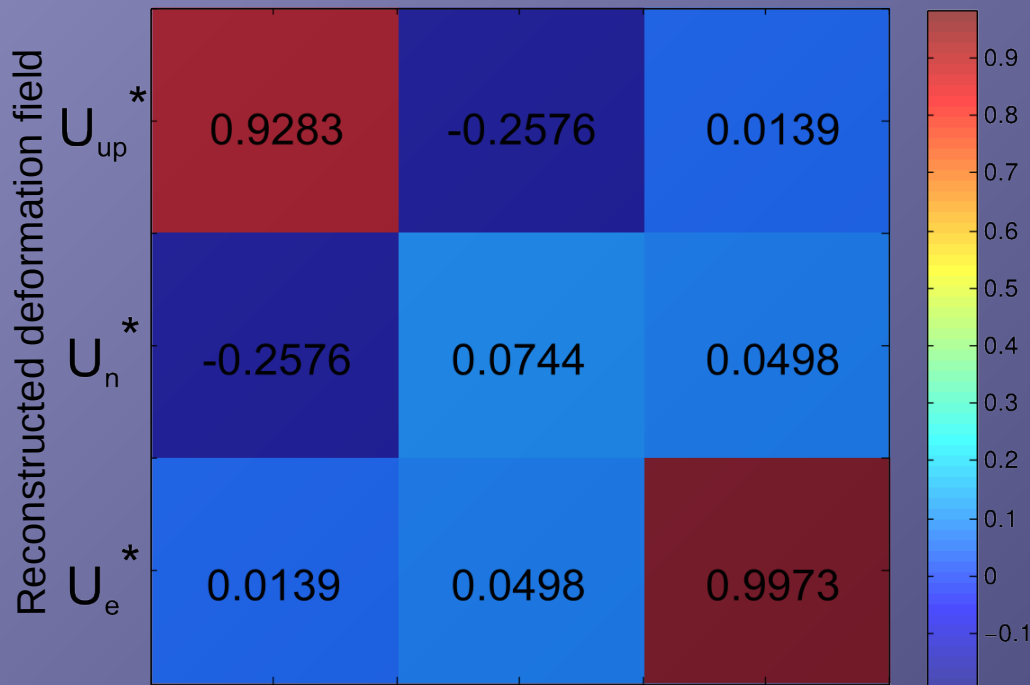
Model Resolution Matrix: Application



Bárðarbunga (Iceland)
CosmoSky-Med data

True deformation field

U_{up} U_n U_e



$$U_{UP}^* = 0.9283 U_{UP} - 0.2576 U_N + 0.0139 U_E$$

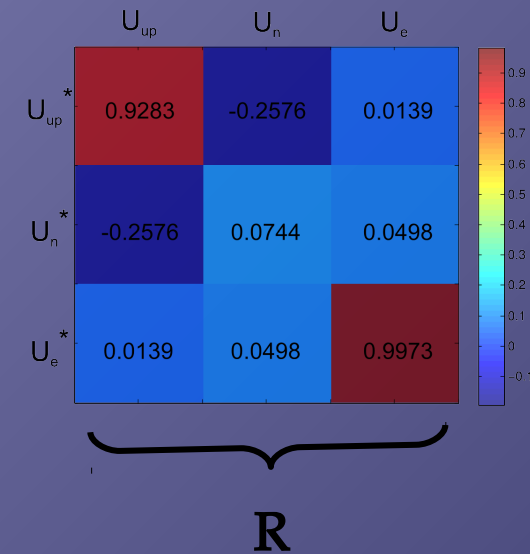
$$U_N^* = -0.2576 U_{UP} + 0.0744 U_N + 0.0498 U_E$$

$$U_E^* = 0.0139 U_{UP} + 0.0498 U_N + 0.9973 U_E$$

Inversion

General solution of the linear inverse problem:

$$\mathbf{m}^{est} = \mathbf{G}^{-g} \mathbf{d}^{obs}$$



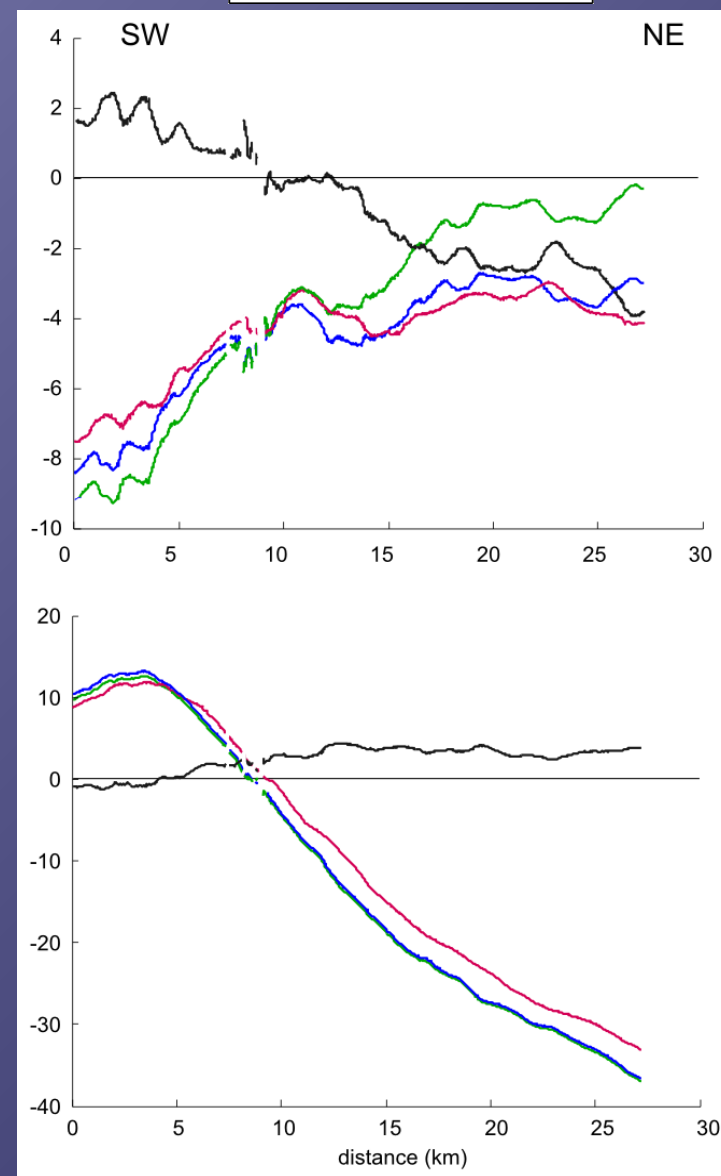
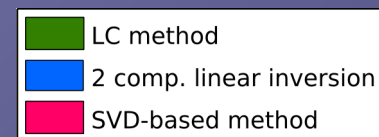
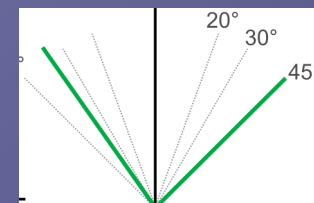
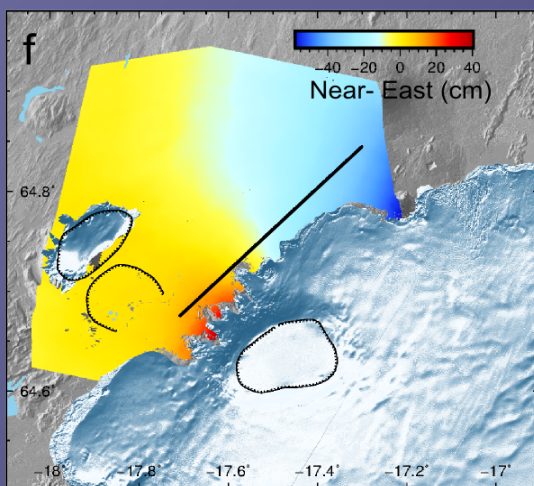
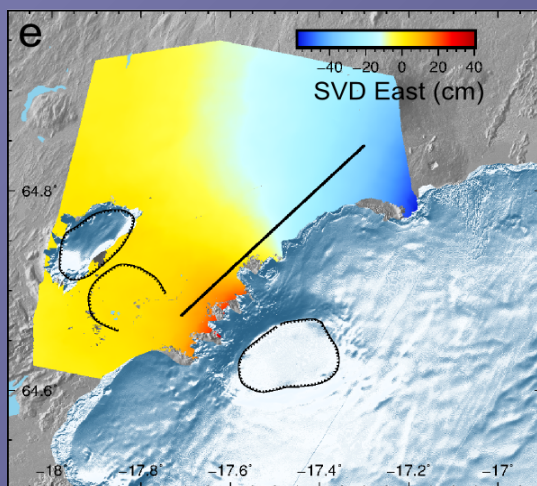
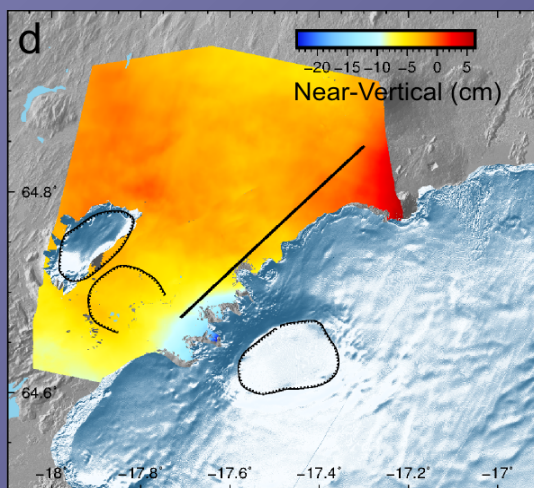
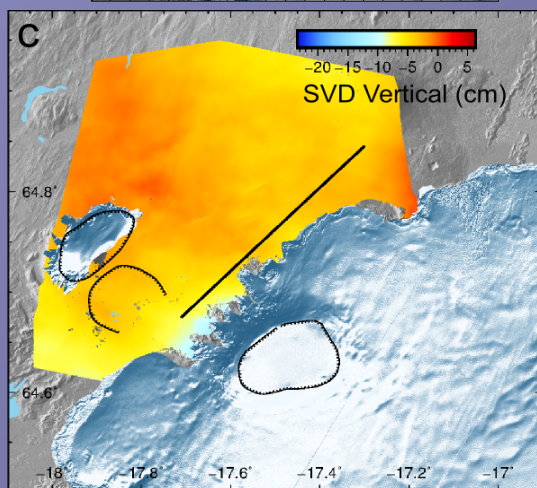
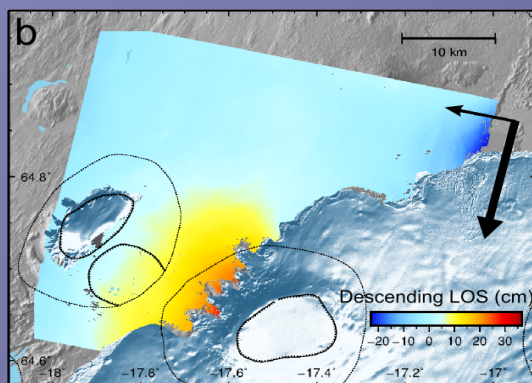
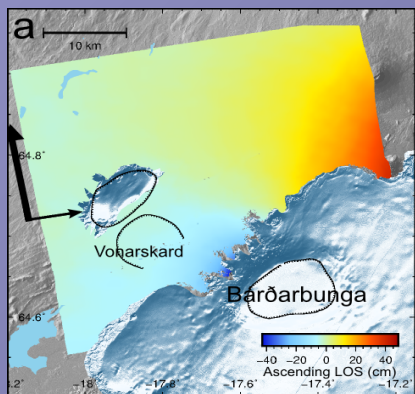
\mathbf{G} is decomposed using a SVD.

To construct the general inverse we truncate the initial decomposition by taking into account only the eigenvalues containing information.

The general inverse can be written as follow (Menke, 1989):

$$\mathbf{m}^{est} = \underbrace{\mathbf{V}_p \mathbf{\Lambda}_p^{-1} \mathbf{U}_p^T}_{\mathbf{G}^{-g}} \mathbf{d}^{obs}$$

Bárðarbunga



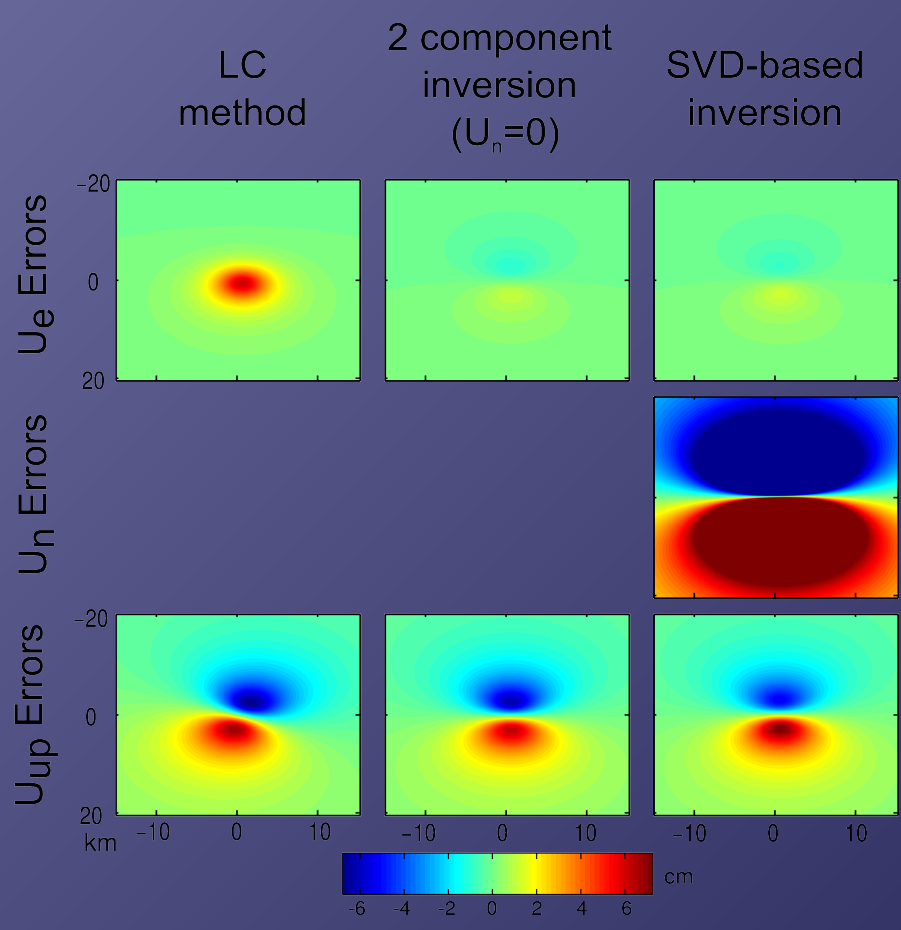
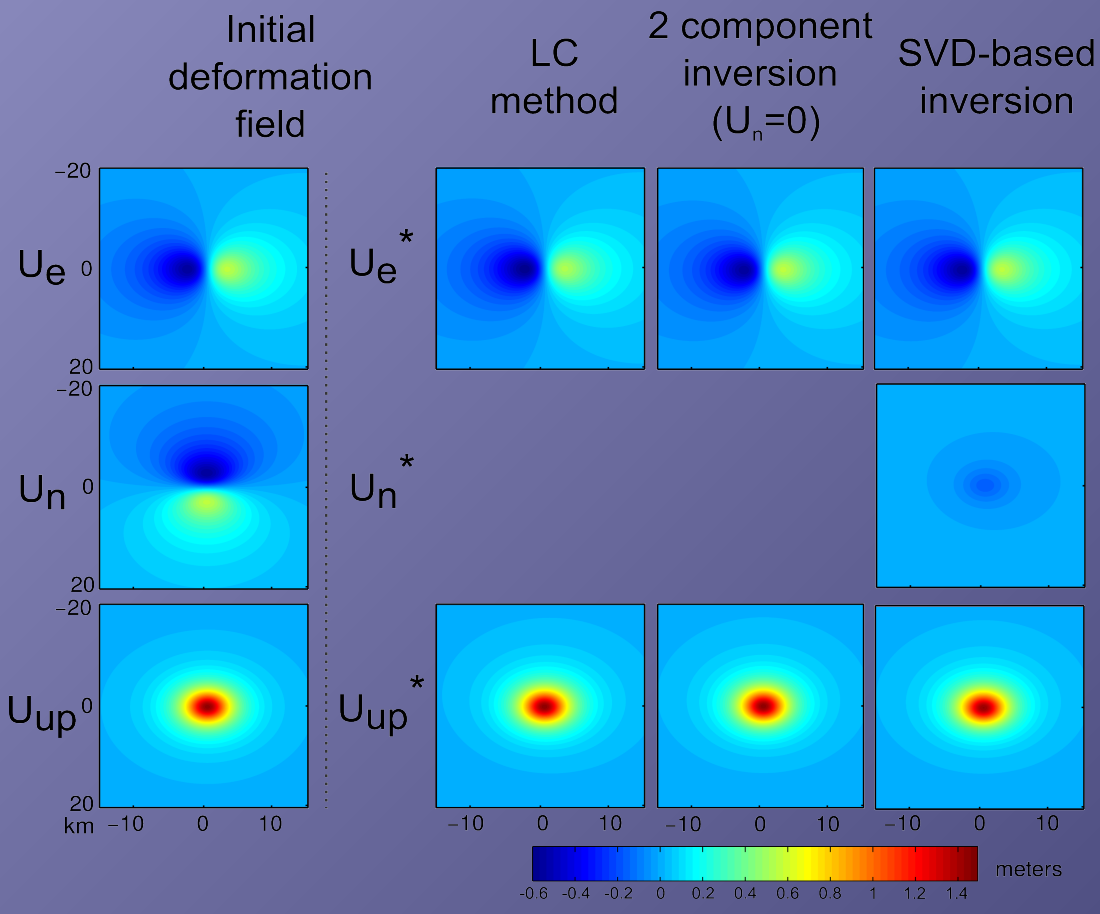
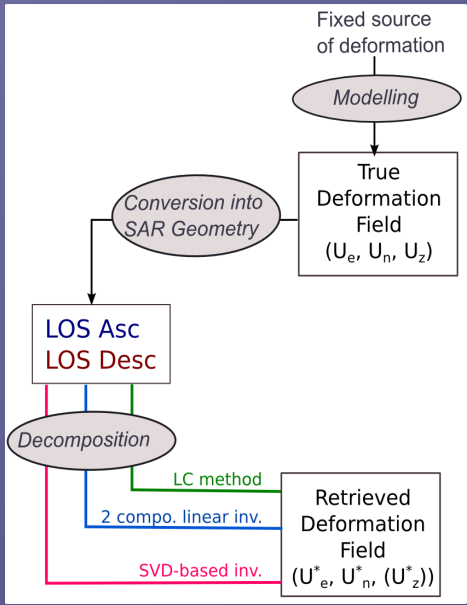
Interferograms

Retrieved Vertical component

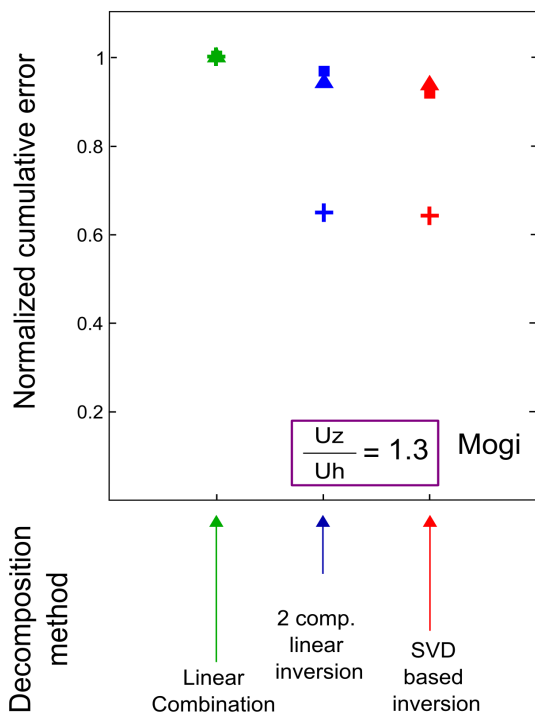
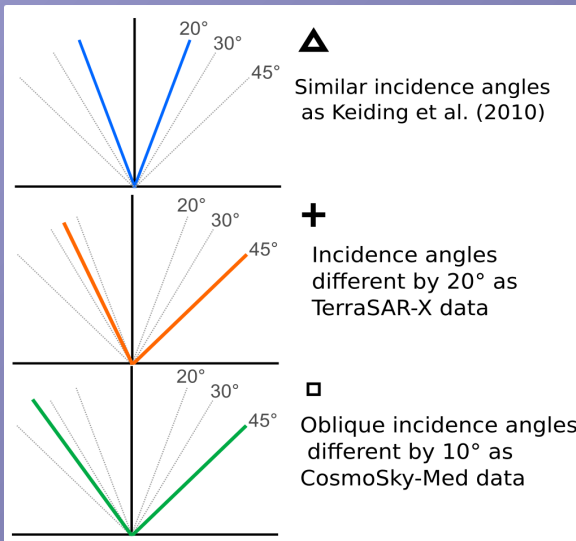
Retrieved East component

Comparison using Simulations

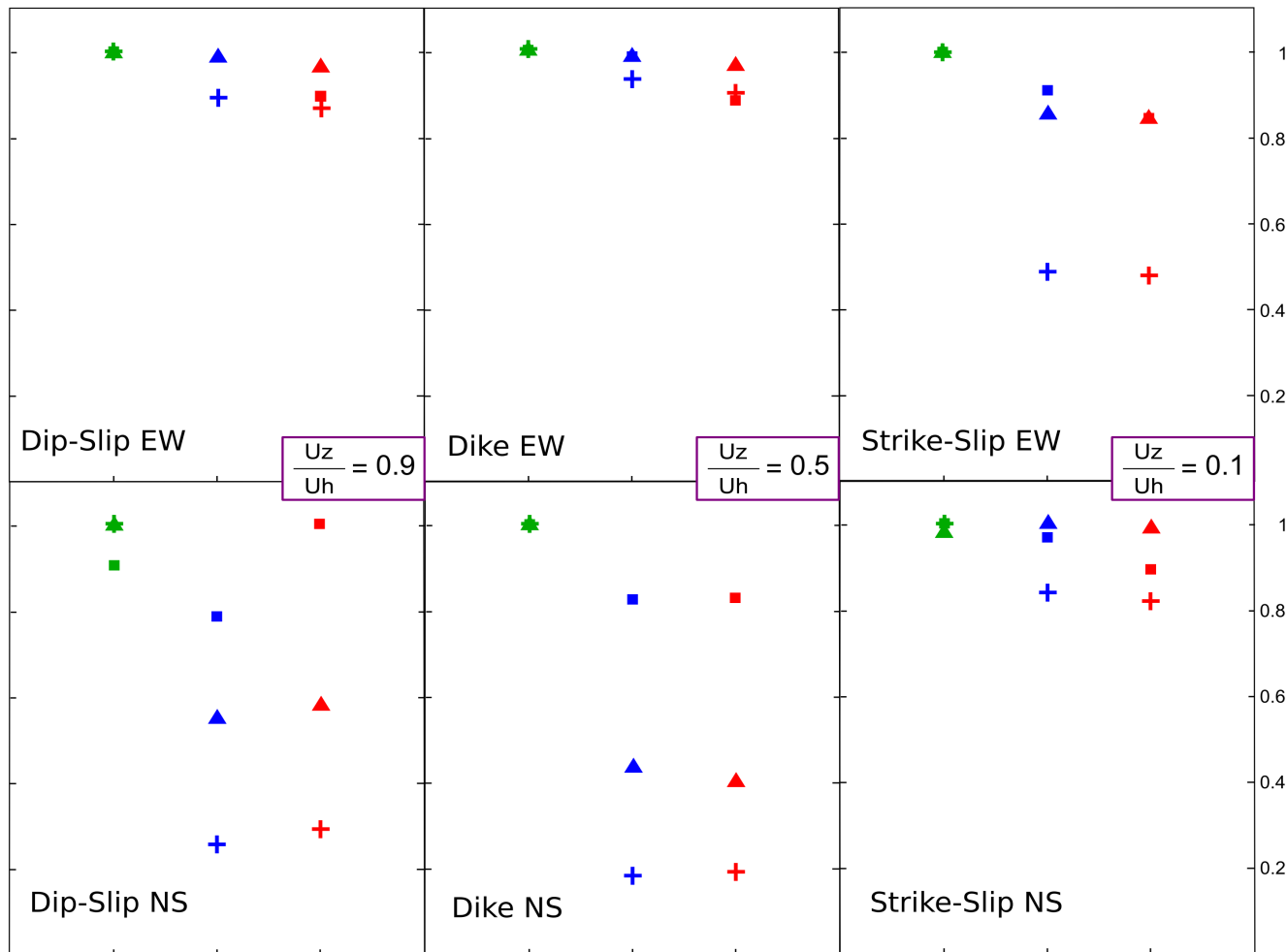
Mogi source: $dV = 0.1 \text{ km}^3$
 $Z = 4 \text{ km}$



Detailed comparison: U_z

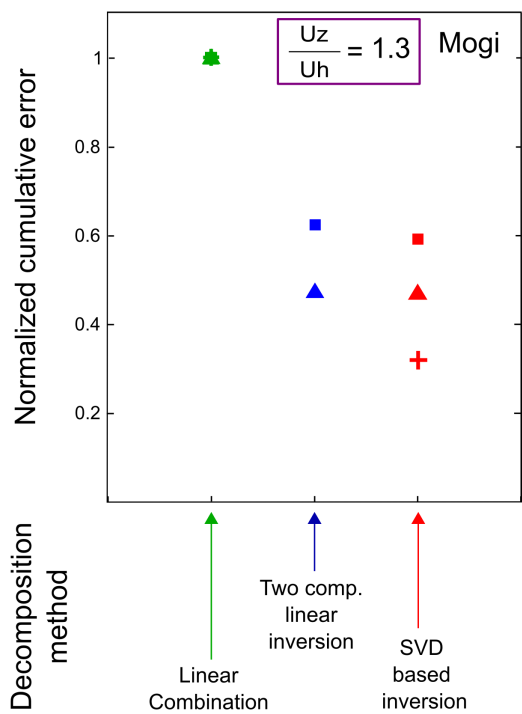
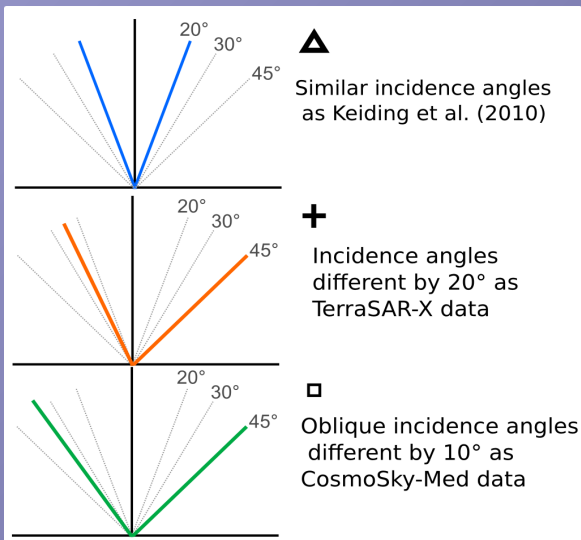


Retrieved Vertical component

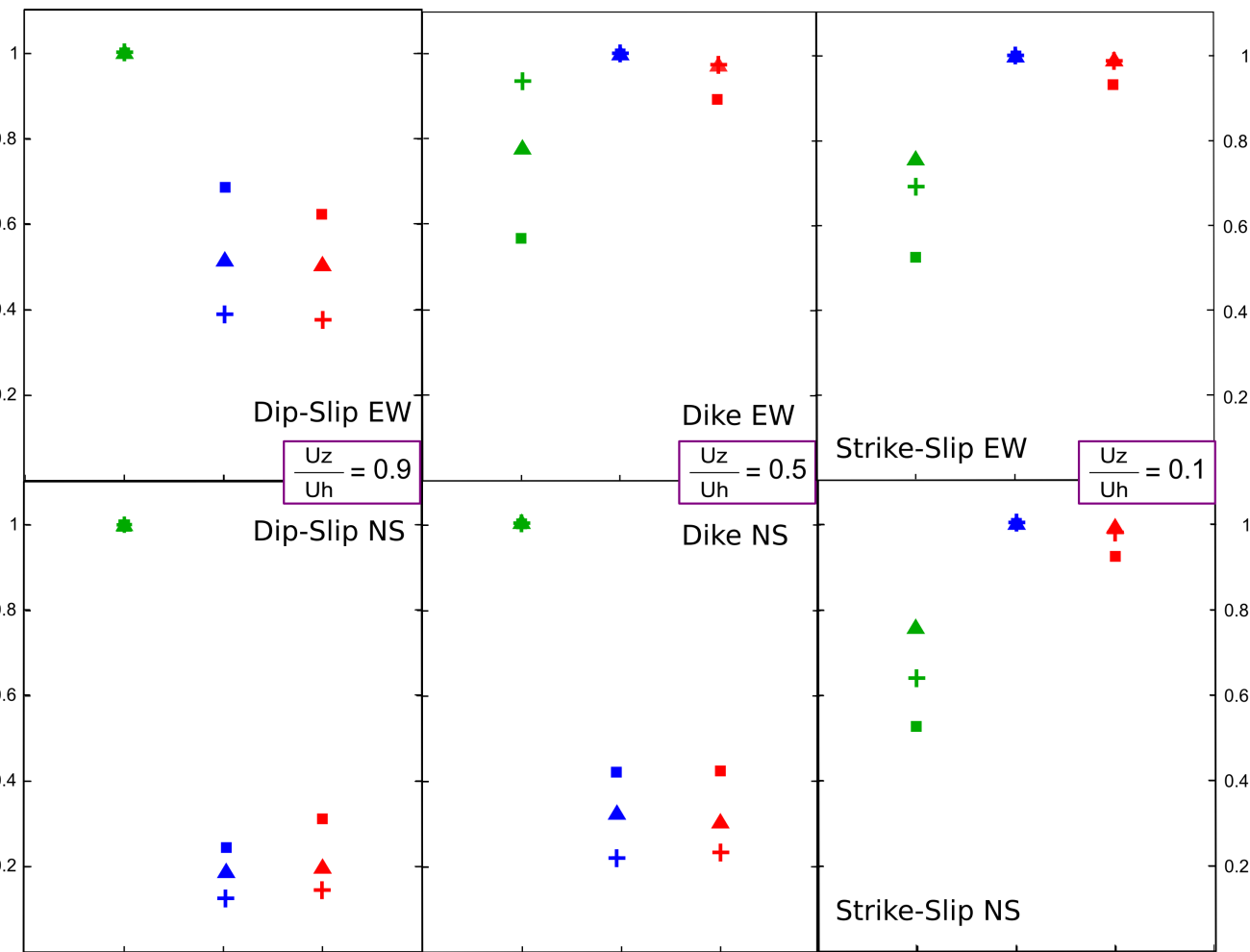


Decrease in the Vertical component / Increase in the horizontal components

Detailed comparison: U_E

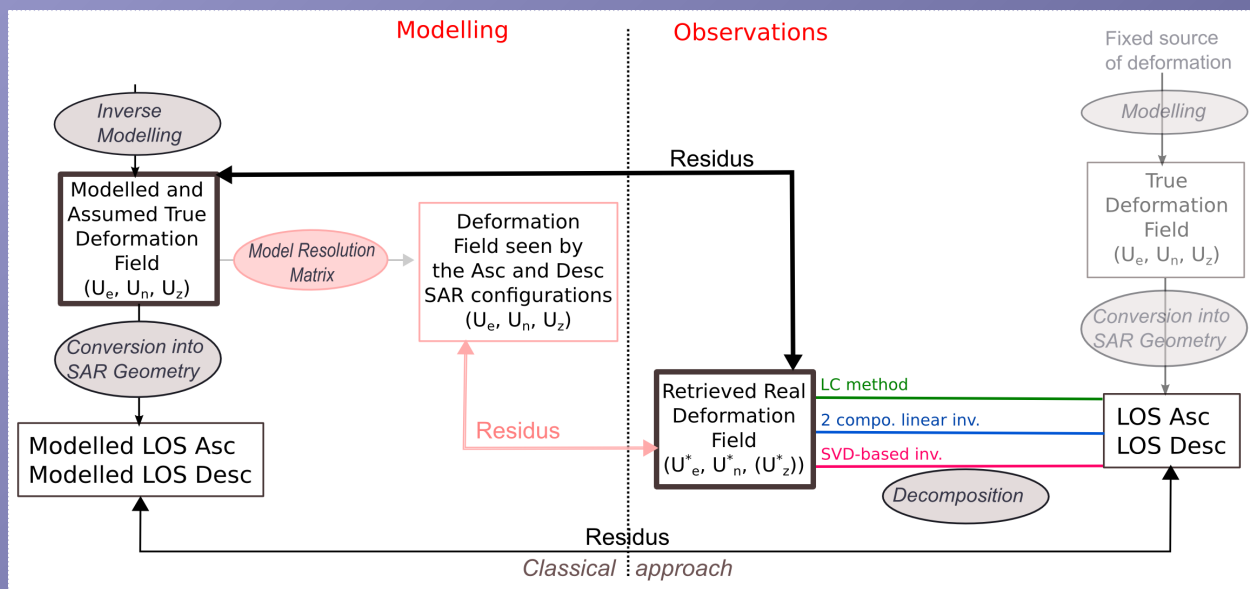


Retrieved East component



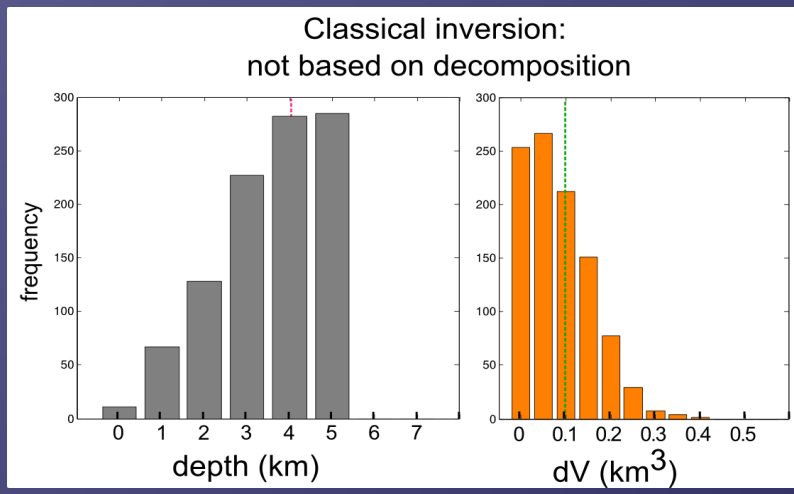
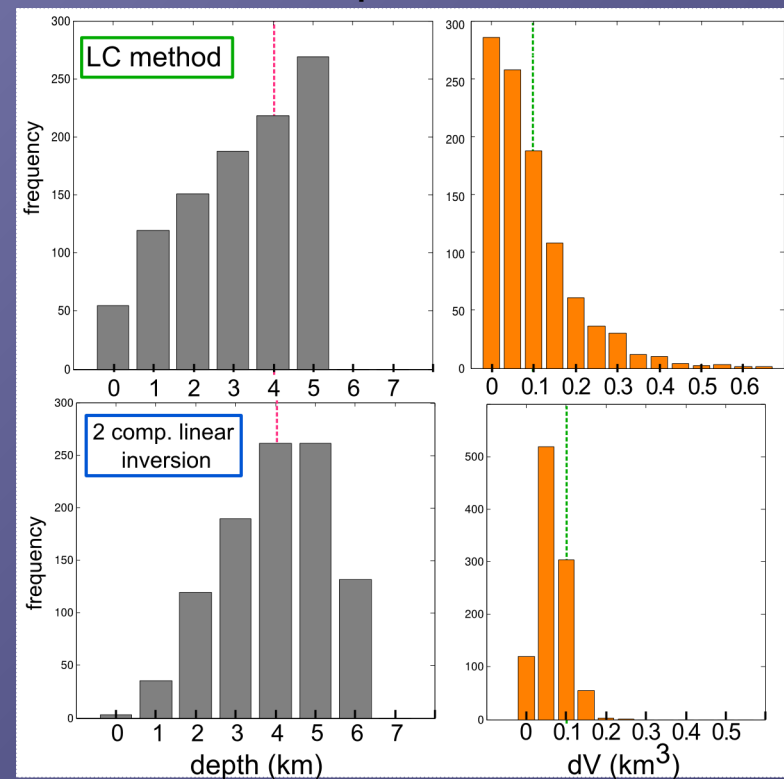
Decrease in the Vertical component / Increase in the horizontal components

Comparison using simple Modelling

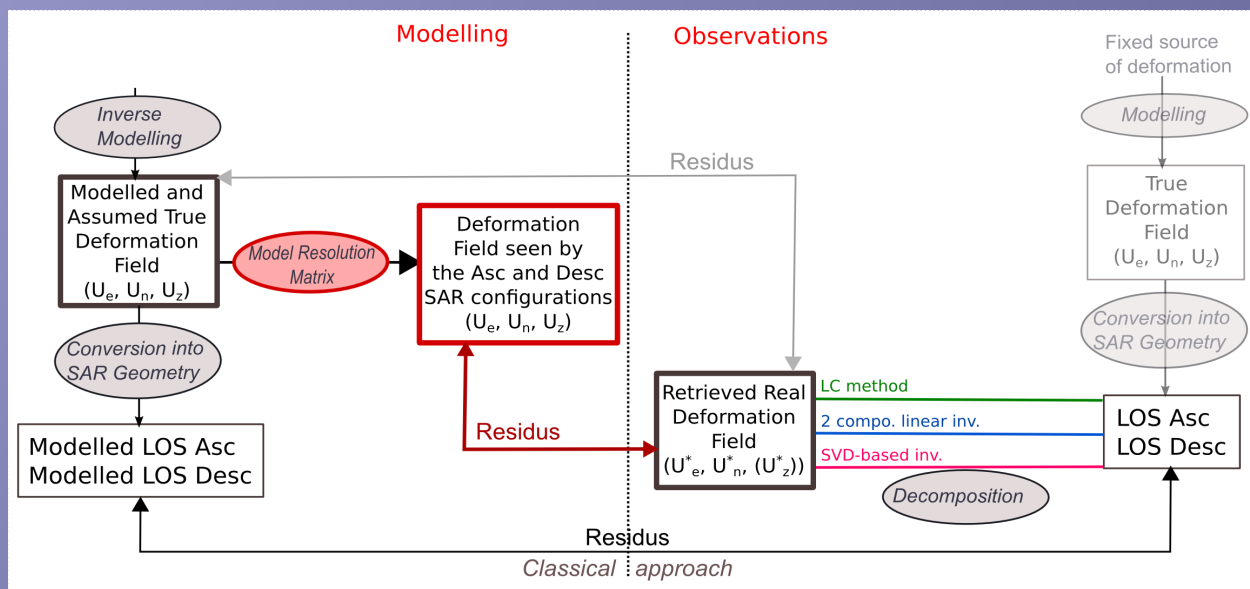


Mogi source: $dV = 0.1 \text{ km}^3$
 $Z = 4 \text{ km}$

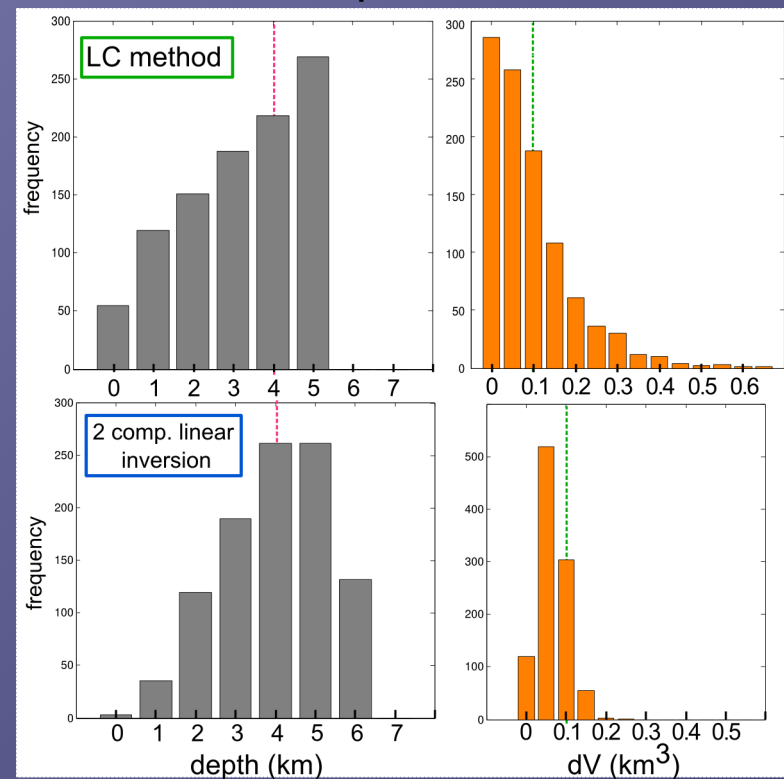
Modelling based on Decomposition methods



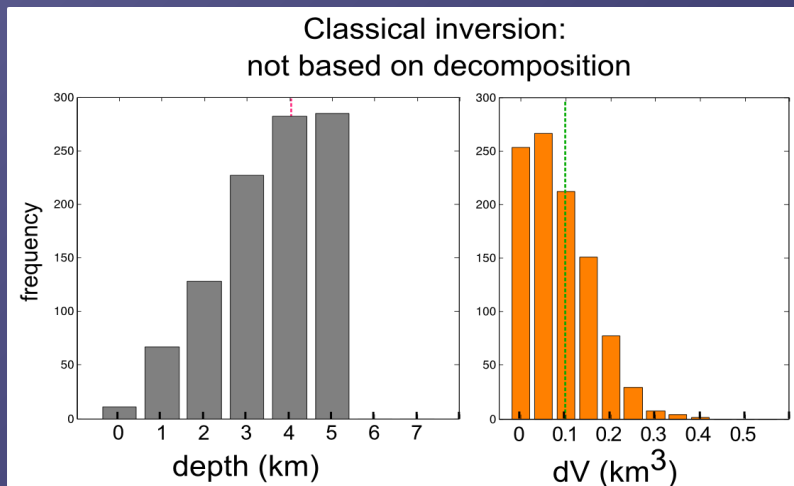
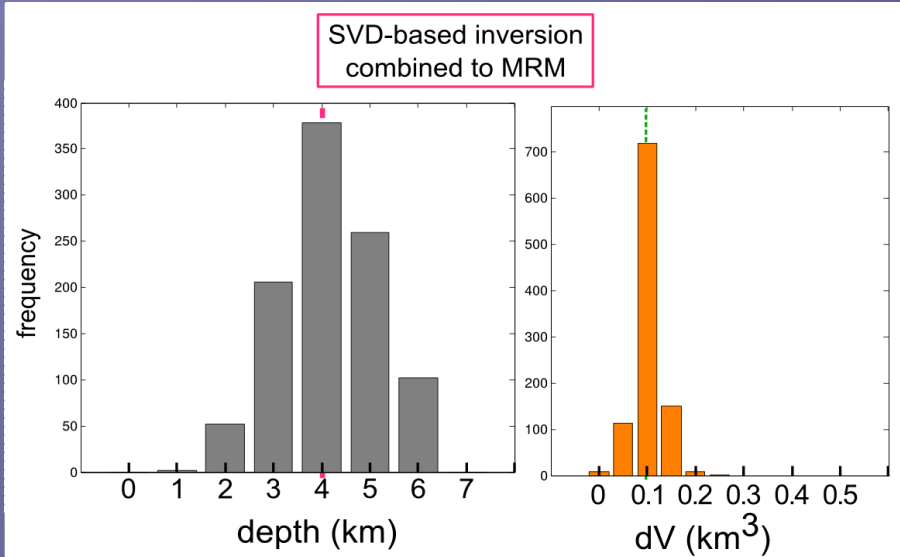
Comparison using simple Modelling



Modelling based on Decomposition methods



Mogi source: $dV = 0.1 km^3$
 $Z = 4 km$



Summary

- Decomposition results will depend on: the combined viewing geometries, the deformation field and the orientation of its source.
- Mixed incidence angles, contributes to reduce errors on the reconstructed east and vertical components
- LC method: not particularly recommended
- Model resolution matrix quantifies the uncertainties on the true deformation field measurement and can be used for better constraining models.